

$$\begin{aligned} p^0(0) &= a_0^0 & &= p_0 \\ p^0(T) &= a_0^0 + a_1^0 T + a_2^0 T^2 + a_3^0 T^3 & &= p_1 \\ \dot{p}^0(0) &= a_1^0 & &= 0 \\ \dot{p}^0(T) - \dot{p}^1(0) &= a_1^0 + 2a_2^0 T + 3a_3^0 T^2 - a_1^1 & &= 0 \\ \ddot{p}^0(T) - \ddot{p}^1(0) &= 2a_2^0 + 6a_3^0 T - 2a_2^1 & &= 0 \end{aligned}$$

$$\begin{aligned} p^n(0) &= a_0^n & &= p_n \\ p^n(T) &= a_0^n + a_1^n T + a_2^n T^2 + a_3^n T^3 & &= p_{n+1} \\ \dot{p}^n(T) &= a_1^n + 2a_2^n T + 3a_3^n T^2 & &= 0 \end{aligned}$$

$$A(T) \vec{a} = p_0 \text{ where}$$

A hand-drawn diagram on lined paper showing a network topology. A central node is connected to several peripheral nodes, forming a star-like structure. A large bracket is drawn on the right side of the diagram.

* if done correctly, "spline" function may do this.

Resolved Rate Trajectory Generation:

• Just finished covering techniques to connect initial and desired end-effector configuration with a trajectory using splines & inverse kinematics.

Problems: 1) multiple solns to inverse kinematics can cause problems
2) redundant arms do have unique/finite inverse

So, to avoid these problems, let's consider an alternative technique called resolved rate trajectory generation.

Given a desired end-effector trajectory $g_e^*(t)$ and its associated velocity

$(\dot{g}_e^*)^b(t)$, we consider

$$(\dot{g}_e^*)^b(t) = J^b(\alpha(t)) \dot{\alpha}(t)$$

in order to solve for $\dot{\alpha}(t)$.

\Rightarrow leads to differential equation:

$$\dot{\alpha}(t) = (J^b(\alpha(t)))^\# (\dot{g}_e^*)^b$$

with initial condition:

$$\alpha(0) = \text{inv. kin. } g_e^*(0) = \alpha_0 \rightarrow \text{usually we know this upfront.}$$

* at this point / we just need to integrate to get the solution.

Ideally, let a computational program deal with this, but if the option is not available, here is one option - - -

$$\dot{\alpha}(t) = (J^b(\alpha(t)))^\# (\dot{g}_e^*)^b \quad \text{--- discretize time}$$

↓

discretize derivative

$t_0, t_1, \dots, t_n, t_f$
where $t_{i+1} - t_i = \Delta t$

(should be small.)

$$\dot{\alpha}(t_{ic}) = \frac{\alpha(t_{i+1}) - \alpha(t_i)}{\Delta t}$$

$$\Rightarrow \frac{\alpha(t_{i+1}) - \alpha(t_i)}{\Delta t} = \cancel{\dot{\alpha}(t_{ic})} = \left(J^b(\alpha(t_i)) \right)^\# (\dot{g}_e^*)^b$$

$$= (J^b(\alpha(t_k)))^\# (\dot{g}_e^*(t_k))^b$$

$$\Rightarrow \alpha(t_{k+1}) = \alpha(t_k) + \Delta t (J^b(\alpha(t_k)))^\# (\dot{g}_e^*(t_k))^b$$

→ repeat for all $t_k, k=0, \dots, n+1$

- This is a first-order accurate integration technique; there are other more accurate methods.
- Assumes we can get $(\dot{g}_e^*(t))^b$ from a continuous trajectory $g_e^*(t)$.

So, suppose that $g_e^*(t)$ is really just a collection of closely spaced way-points for which $(\dot{g}_e^*(t))^b$ can't be found, e.g. we just have $g_e^*(t_k)$.

NAIVE APPROACH: If $g_e^*(t_k)$ is vectorizable, then use standard Jacobian and first order approximation to end-effector derivative:

$$\dot{\alpha}(t_{k+1}) = \dot{\alpha}(t_k) + \Delta t J^\#(\alpha(t_k)) \frac{g_e^*(t_{k+1}) - g_e^*(t_k)}{\Delta t}$$

$$\Rightarrow \alpha(t_{k+1}) = \alpha(t_k) + J^\#(\alpha(t_k)) (g_e^*(t_{k+1}) - g_e^*(t_k))$$

Geometric Approach: use logarithm,

$$\left(\xi_k^*(t_k) \right)^b = \ln_{\Delta t} \left(g^{-1}(t_k) g(t_{k+1}) \right)$$

\parallel
 ξ_k

\hat{L} need the time part to be Δt ,
eg., set $\tau = \Delta t$

\Rightarrow leads to

$$\alpha(t_{k+1}) = \alpha(t_k) + \Delta t \mathcal{J}^b(\alpha(t_k)) \xi_k$$

~~continues~~ continued from last time...

ultimately the idea is to use the Jacobian to relate velocities, then integrate up to final configuration of the trajectory (MATLAB & others can do this)

Problem 1: If true trajectory starts to deviate from desired, then end-effector may diverge from desired trajectory (open-loop problem)

Problem 2: What if the trajectory crosses, or passes nearby, a singularity? At singularity, Jacobian loses rank.

What happens to $J^{\#}$?

→ main part of $J^{\#}$ is $(JJ^T)^{-1}$

$$\det(A) = \prod \lambda_i$$

losing rank $\Rightarrow \lambda_i \rightarrow 0$ for some i

\Rightarrow inverse matrix blows up!

\Rightarrow get ∞ velocities.

• Observation: when minimizing joint velocities, the pseudo-inverse gives all joints velocities the same weight. May not be desirable.

Damped Pseudo-Inverse

• GOAL: avoid blow-up near singularities.

the pseudo-inverse solved for the \dot{x} that minimized

$$L(\dot{x}) = \|\dot{x}\| \quad \text{subject to } \dot{y} = J(x)\dot{x}$$

(for redundant/sufficient)

leads to blow-up since $\dot{\mathbf{q}}^b = \mathbf{J}^b(\alpha) \dot{\alpha}$ must hold.

Propose instead, to minimize

$$\mathcal{L}(\dot{\alpha}) = \frac{1}{2} \|\dot{\mathbf{q}}^b - \mathbf{J}^b(\alpha) \dot{\alpha}\|^2 + \frac{1}{2} \rho^2 \|\dot{\alpha}\|^2$$

The solution is called the damped pseudo-inverse and is

$$\dot{\alpha} = (\mathbf{J}^b(\alpha))^{\#} \dot{\mathbf{q}}^b \quad \text{with} \quad (\mathbf{J}^b(\alpha; \rho))^{\#} = (\mathbf{J}^b)^T (\mathbf{J}^b (\mathbf{J}^b)^T + \rho^2 \mathbf{I})^{-1}$$

eigenvalues of $(\mathbf{J}^b \mathbf{J}^b)^T$ change from $\frac{1}{\sigma_i^2}$ to $\frac{\sigma_i^2}{\sigma_i^2 + \rho^2}$

the issue will be that now the joint velocities are bounded.

$$\text{In fact, } \frac{\|\dot{\alpha}\|}{\|\dot{\mathbf{q}}^b\|} \leq \frac{1}{2\rho}$$

trajectory may deviate.

Weighted Pseudo-Inverse

• This considers an alternative formulation of the pseudo-inverse minimization problem.

It is the minimization of

$$\|\mathbf{a}\|^2 = \mathbf{a} \cdot \mathbf{a} = \mathbf{a}^T \mathbf{a}$$

$$\mathcal{L}(\dot{\alpha}) = \frac{1}{2} \|\dot{\mathbf{q}}^b - \mathbf{J}^b(\alpha) \dot{\alpha}\|^2 + \frac{1}{2} \|\dot{\alpha}\|_W^2$$

$$\text{where } \|\mathbf{v}\|_W = \mathbf{v}^T \mathbf{W} \mathbf{v}$$

and \mathbf{W} is positive definite

& symmetric.

Solution to this problem is:

$$\dot{\alpha} = W^{-1}(J^b)^T (J^b W^{-1}(J^b)^T)^{-1} \xi^b$$

in redundant/sufficient case.

- now we can give different joint angle rates different ~~per~~ priorities.

So, $J^\# = W^{-1}(J^b)^T (J^b W^{-1}(J^b)^T)^{-1}$ is the weighted pseudo-inverse.

Side note: Damped - Weighted Pseudo-Inverse:

$$J^\# = W^{-1}(J^b)^T (J^b W^{-1}(J^b)^T + \rho^2 \mathbf{I})^{-1}$$

HW info:

ode45 (____, tspan, I.c.)

$$\dot{\alpha}(t) = (J^b(\alpha(t)))^\# \xi^b$$

function alphadot = diffeq(alpha, t)

$$\dot{\alpha} = (J^b(\alpha(t)))^\# \xi^b(t)$$

end

~~Plot the results~~