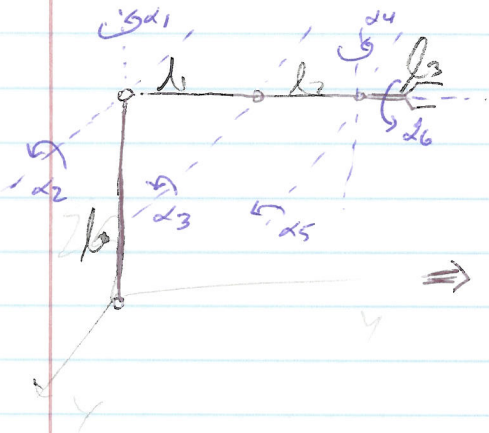


last part of inverse kinematics:

get final angle such that $\theta_{des} = \alpha_1 + \alpha_2 + \alpha_3$

$$\Rightarrow \alpha_3 = \theta_{des} - \alpha_1 - \alpha_2$$

Inverse kinematics of Elbow manipulator (Algebraic Method)



this approach uses Piepe's method.

$$g_e(\alpha) = g_1(\alpha_1) g_2(\alpha_2) g_3(\alpha_3) g_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6) g_7$$

\Rightarrow Split

$$g_e(\alpha) = \underbrace{g_1(\alpha_1) g_2(\alpha_2) g_3(\alpha_3) \bar{g}_4}_{\text{position}} \underbrace{\tilde{g}_4(\alpha_4) \tilde{g}_5(\alpha_5) \tilde{g}_6(\alpha_6) g_7}_{\text{reorientation}}$$

can position anywhere! allows for arbitrary
in the appropriate workspace! reorientation
no control over orientation! (no translation)

constant
transfer motion.

We have some desired end-effector configuration g_e^* .
Move constant g_7 term to right hand side

$$g_e^* g_7^{-1} = g_1(\alpha_1) g_2(\alpha_2) g_3(\alpha_3) \bar{g}_4 \tilde{g}_4(\alpha_4) \tilde{g}_5(\alpha_5) \tilde{g}_6(\alpha_6)$$

define $g_w^* = g_e^* g_7^{-1}$

find $(\alpha_1, \alpha_2, \alpha_3)$ such that

$$\text{position}(g_w^*) = \text{position}(g_1(\alpha_1) g_2(\alpha_2) g_3(\alpha_3) \bar{g}_4)$$

If we define

$$g_w(\alpha) = g_1(\alpha_1) g_2(\alpha_2) g_3(\alpha_3) g_4$$

then

$$g_w(\alpha) = \begin{bmatrix} R_w(\alpha_1, \alpha_2, \alpha_3) & d_w(\alpha_1, \alpha_2, \alpha_3) \\ 0 & 1 \end{bmatrix}$$

and

$$\text{position}(g_w(\alpha)) = d_w(\alpha_1, \alpha_2, \alpha_3) = \begin{Bmatrix} x_w \\ y_w \\ z_w \end{Bmatrix}$$

$$\begin{Bmatrix} x_w \\ y_w \\ z_w \end{Bmatrix} = \begin{Bmatrix} -(l_1 \cos(\alpha_2) + l_2 \cos(\alpha_2 + \alpha_3)) \sin(\alpha_1) \\ (l_1 \cos(\alpha_2) + l_2 \cos(\alpha_2 + \alpha_3)) \cos(\alpha_1) \\ l_0 + l_1 \sin(\alpha_2) + l_2 \sin(\alpha_2 + \alpha_3) \end{Bmatrix}$$

↑ can shift origin up to remove.

Algebraic Approach:

- try to solve simultaneous equations
- elimination theory.
 - successively eliminate variables until a single equation in one unknown is achieved.
 - for manipulator forward kinematics equations, there exists a systematic approach to carry out this procedure.
 - back-substitution gives solution.

$$\begin{aligned} (x_w^*)^2 + (y_w^*)^2 + (z_w^* - l_0)^2 &= x_w^2(\alpha_1, \alpha_2, \alpha_3) + y_w^2(\alpha_1, \alpha_2, \alpha_3) + (z_w(\alpha_1, \alpha_2, \alpha_3) - l_0)^2 \\ &= l_1^2 + l_2^2 - 2l_1l_2 \cos(\alpha_3) \\ \Rightarrow \cos(\alpha_3) &= \frac{(x_w^*)^2 + (y_w^*)^2 + (z_w^* - l_0)^2 - l_1^2 - l_2^2}{2l_1l_2} \end{aligned}$$

→ two solutions to inverse cosine.

next, we also should have $\alpha_1, \alpha_2, \alpha_3$ satisfy:

I want to find $(\alpha_1, \alpha_2, \alpha_3)$ such that:

$$\begin{aligned}(x_w^*)^2 + (y_w^*)^2 &= x_w^2(\alpha_1, \alpha_2, \alpha_3) + y_w^2(\alpha_1, \alpha_2, \alpha_3) \\ &= (l_1 \cos(\alpha_2) + l_2 \cos(\alpha_2 + \alpha_3))^2\end{aligned}$$

$$\text{define } r = \sqrt{(x_w^*)^2 + (y_w^*)^2}$$

$$\Rightarrow r = (l_1 + l_2 \cos(\alpha_3)) \cos(\alpha_2) - (l_2 \sin(\alpha_3)) \sin(\alpha_2)$$

what is α_2 ? we know α_3 already.

apply change of variable using $w = \tan\left(\frac{1}{2}\alpha_2\right)$
 [because $\cos(\alpha_2) = \frac{1-w^2}{1+w^2}$ and $\sin(\alpha_2) = \frac{2w}{1+w^2}$]

$$\Rightarrow r = (l_1 + l_2 \cos(\alpha_3)) \frac{1-w^2}{1+w^2} - \frac{(2 l_2 \sin(\alpha_3)) w}{1+w^2}$$

10/17/07

241

ECE 4560

continued from Monday

$$(1 + w^2)r = (l_1 + l_2 \cos(\alpha_3))(1 - w^2) - 2l_2 \sin(\alpha_3)w$$

$$\Rightarrow (r + l_1 + l_2 \cos(\alpha_3))w^2 - 2l_2 \sin(\alpha_3)w + (r - l_1 - l_2 \cos(\alpha_3)) = 0$$

↑ quadratic equation, can be solved using quadratic formula.

given solution for α_3 , can solve for w and then use that to solve for α_2 using $\tan(\frac{1}{2}\alpha_2) = w$

→ solve using both solutions to α_3 .

→ the quadratic formula gives two solutions per equation there are four potential solutions.

let's worry about these later.

Lastly, to get α_1 , we want to find the solution to

$$\left. \begin{aligned} \sin(\alpha_1) &= -\frac{x_w^*}{l_1 \cos(\alpha_2) + l_2 \cos(\alpha_2 + \alpha_3)} \\ \cos(\alpha_1) &= \frac{y_w^*}{l_1 \cos(\alpha_2) + l_2 \cos(\alpha_2 + \alpha_3)} \end{aligned} \right\}$$

$$\alpha_1 = \text{atan2}(\cos(\alpha_1), \sin(\alpha_1)) = \text{atan2}(y_w^*, x_w^*)$$

One solution

Now, go back to the four solutions & pick a correct one.

do that by plugging it in and verifying that

$$x_w^* = x_w(\alpha_1, \alpha_2, \alpha_3)$$

$$y_w^* = y_w(\alpha_1, \alpha_2, \alpha_3)$$

$$z_w^* = z_w(\alpha_1, \alpha_2, \alpha_3)$$

24-2

* once the wrist is positioned, the next step is to get orientation correct.

$$g_e^* = g_1(\alpha_1^*) g_2(\alpha_2^*) g_3(\alpha_3^*) g_4(\alpha_4) \tilde{g}_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6) g_7$$

$$g_w^{-1} g_e^* = g_w \tilde{g}_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6) g_7 g_7^{-1}$$

$$g_w^{-1} g_e^* g_7^{-1} = \tilde{g}_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6)$$

$$g_w^{-1} g_w^* = \tilde{g}_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6)$$

If our work is correct, then

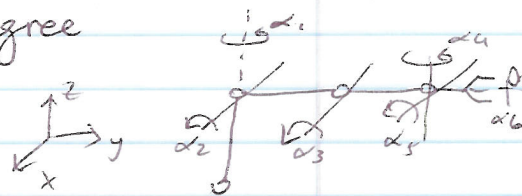
$$g_w^{-1}(\alpha_1, \alpha_2, \alpha_3) g_w^* = \begin{bmatrix} R & 0 \\ 0 & 1 \end{bmatrix}$$

and we know that

$$\tilde{g}_4(\alpha_4) g_5(\alpha_5) g_6(\alpha_6) = \begin{bmatrix} R(\alpha_4, \alpha_5, \alpha_6) & 0 \\ 0 & 1 \end{bmatrix}$$

so, we just need to find $\alpha_4, \alpha_5, \alpha_6$ that get the two rotation matrices to agree

What is $R(\alpha_4, \alpha_5, \alpha_6)$?



$$R(\alpha_4, \alpha_5, \alpha_6) = R_z(\alpha_4) R_x(\alpha_5) R_y(\alpha_6)$$

$$R_z(\alpha_4) = \begin{bmatrix} \cos(\alpha_4) & -\sin(\alpha_4) & 0 \\ \sin(\alpha_4) & \cos(\alpha_4) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_x(\alpha_5) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\alpha_5) & -\sin(\alpha_5) \\ 0 & \sin(\alpha_5) & \cos(\alpha_5) \end{bmatrix}$$

$$R_y(\alpha_6) = \begin{bmatrix} \cos(\alpha_6) & 0 & \sin(\alpha_6) \\ 0 & 1 & 0 \\ -\sin(\alpha_6) & 0 & \cos(\alpha_6) \end{bmatrix}$$

$$R_z(\alpha_4) R_x(\alpha_5) = \begin{bmatrix} \cos(\alpha_4) & -\sin(\alpha_4)\cos(\alpha_5) & \sin(\alpha_4)\sin(\alpha_5) \\ \sin(\alpha_4)\cos(\alpha_5) & \cos(\alpha_4)\cos(\alpha_5) & -\cos(\alpha_4)\sin(\alpha_5) \\ 0 & \sin(\alpha_5) & \cos(\alpha_5) \end{bmatrix}$$

$$R_z(\alpha_4) R_x(\alpha_5) R_y(\alpha_6) = \begin{bmatrix} \cos(\alpha_4)\cos(\alpha_6) & -\sin(\alpha_4)\cos(\alpha_5)\cos(\alpha_6) & \cos(\alpha_4)\sin(\alpha_6) \\ -\sin(\alpha_4)\sin(\alpha_5)\sin(\alpha_6) & \cos(\alpha_4)\cos(\alpha_5)\cos(\alpha_6) & -\sin(\alpha_4)\sin(\alpha_6) \\ \sin(\alpha_4)\cos(\alpha_5)\cos(\alpha_6) & \cos(\alpha_4)\sin(\alpha_5)\cos(\alpha_6) & \sin(\alpha_4)\sin(\alpha_6) \\ -\cos(\alpha_5)\sin(\alpha_6) & \sin(\alpha_5) & \cos(\alpha_5)\cos(\alpha_6) \end{bmatrix}$$

Two cases need to be considered,
 1) $\cos(\alpha_5) = 0$, $\sin(\alpha_5) = \pm 1$
 2) $\cos(\alpha_5) \neq 0$

Suppose that we wanted to find $\alpha_4, \alpha_5, \alpha_6$ such that
 $R(\alpha_4, \alpha_5, \alpha_6) = R_z(\alpha_4) \cdot R_x(\alpha_5) R_y(\alpha_6) = R^*$

10/19/07

25-1

ECF 4560

- 1) if $R_{12} = R_{22} = R_{31} = R_{33}$, ~~$R_{32} = \pm 1$~~ $R_{32} = \pm 1$
 then we have $\cos(\alpha_5) = 0$, $\sin(\alpha_5) = \pm 1$
 $\Rightarrow \alpha_5 = \pm \frac{\pi}{2}$

$$R(\alpha_4, \alpha_5, \alpha_6) = \begin{bmatrix} c_4 c_6 \mp s_4 s_6 & 0^{12} & c_4 s_6 \pm s_4 c_6 \\ s_4 c_6 \pm c_4 s_6 & 0^{22} & s_4 s_6 \mp c_4 c_6 \\ 0 & \pm 1^{32} & 0^{33} \end{bmatrix}$$

$$\Rightarrow R(\alpha_4, \alpha_5, \alpha_6) = \begin{bmatrix} \cos(\alpha_4 \pm \alpha_6) & 0 & \sin(\alpha_4 \pm \alpha_6) \\ \sin(\alpha_4 \pm \alpha_6) & 0 & -\cos(\alpha_4 \pm \alpha_6) \\ 0 & \pm 1 & 0 \end{bmatrix}$$

$$Z \times y \Rightarrow \text{if } R_{32} = 1 \Rightarrow \alpha_3 = \frac{\pi}{2}$$

$$\downarrow$$

$$\frac{\pi}{2}$$

$$\alpha_4 + \alpha_6 = \text{atan2}(R_{21}, R_{11})$$

- 2) $R_{32} \neq \pm 1$ and one of R_{21} or R_{22} and one of R_{31} or R_{33} is non-zero,
 $\alpha_4 = \text{atan2}(R_{12}, R_{22})$
 $\alpha_6 = \text{atan2}(-R_{31}, R_{33})$
 $\alpha_5 = \text{asin}(R_{32})$

So, we determined $\alpha^* = (\alpha_1^*, \alpha_2^*, \alpha_3^*, \alpha_4^*, \alpha_5^*, \alpha_6^*)$

Such that $g_e(\alpha^*) = g_e^*$

- 1) Break up forward kinematics into wrist position & hand orientation.
- 2) Solve for wrist position
- 3) " " hand orientation.

MANIPULATOR JACOBIAN

• The manipulator Jacobian gives the end-effector velocity as a function of the joint configuration and the joint velocity.

• There's a generic definition available, but we are going to take advantage of the structure of the forward kinematics to compute the Jacobian.

- 1) Product of Lie groups
- 2) ~ " exponential.